

# THE MATHEMATICAL MODELLING AND PERFORMANCE EVALUATION OF PAINT MANUFACTURING SYSTEM USING FUZZY RELIABILITY APPROACH

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## ABSTRACT

*In the present paper, we present a novel method for performance evaluation of a paint manufacturing plant in which five subsystems are connected in series configuration. The mathematical modelling of the system is carried out using the mnemonic rule to formulate C-K differential difference equations. The concept of fuzzy reliability, coverage factor and constant failure and repair densities have been used to analyze the availability and performance of the system. Finally, for a particular case numerical results for fuzzy availability and profit function has been derived with respect to time.*

**KEYWORDS:** Paint Manufacturing Plant, Fuzzy Availability, Mnemonic Rule & Coverage Factor

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## INTRODUCTION

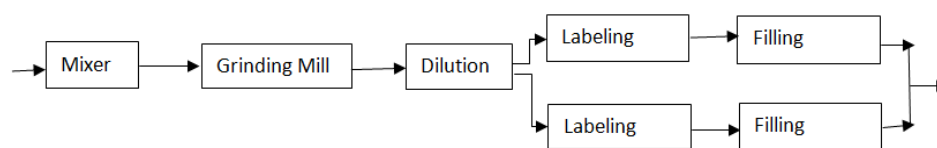
Availability, busy period of repairman and profit function are always consider the key indices of performance analysis of engineering systems. It remains a hot topic of discussion from decades among the researcher. A lot of literature related to availability analysis of engineering systems have been exist. Relevant literature can be found Barlow and Proschan (1965), Cui and Xie (2001), Ram (2013), and Qiu and Cui (2018). Kumar and Malik (2014) evaluated reliability of a computer system with priority to H/W repair over replacement of H/W and up-gradation of S/W subject to MOT and MRT. Most of studies carried out so far based on the conventional approach of reliability theory, i.e., binary state assumption. The system is either operative or failed. Sharma and Khanduja (2013) carried out the performance and availability evaluation of a sugar plant using conventional reliability approach. Kumar et al. (2018) also studied a stochastic model of non-identical redundant systems with priority and preventive maintenance. But, the conventional reliability approach has not extensively acceptable in current engineering systems. Zadeh (1965) presented the basic concepts of fuzzy set theory by giving higher importance to scientific environment. The basic scenario in reliability engineering and it can easily handle all the states that fall between working and failed state. The wide coverage of fuzzy state assumption replaces the conventional reliability theory.

Kaufmann (1975) emphasized on the applications of fuzzy reliability in engineering systems by introducing component failure possibility instead of failure probability. Singer (1990) suggested a new methodology for finding reliability measures by considering repair and failure time variables as triangular fuzzy numbers. Mishra (1992) tried to couple the traditional lambda- $\tau$  method with fuzzy set theory to analyze fuzzy reliability of repairable systems.

Cai et al. (1993) proposed fuzzy state as a basis of fuzzy reliability. Fuzzy number arithmetic operations have been used in fuzzy reliability evaluation by Chen (1994). Zuang (1995) analyzed reliability of a system presented by associating the fuzziness to various parameters. Komal et al. (2009, 2010) and Kumar et al. (2012) used these methodologies to assess the reliability of butter–oil, paper, and fertilizer manufacturing plants, waste clean-up manipulator. Time dependent fuzzy sets for reliability evaluation has been introduced by Aliev and Kara (2004). Chen (2003) introduced the vague sets methodology for obtaining fuzzy system reliability. And, Jiang et al. (2007) applied it for reliability evaluation of Mirrored Disk Organizations. Aggarwal et al. (2014) studied the availability and performance of a butter oil production system. Aggarwal et al. (2016) formulated a mathematical model and obtained the results for reliability of the serial processes in feeding system of sugar plant. Li et al. (2017) developed a system reliability analysis method based on fuzzy probability. Kumar and Saini (2017) formulated a mathematical model for a sugar plant using fuzzy reliability approach. The overall performance of an industrial system depends on the availability of the system. Many researcher like Kachitvichyanukul (2012), Sharma and Vishwakarma (2014), etc. used many techniques such as GA, PSO, Markovian and DE algorithms for the performance evaluation of industrial systems. Though, a lot of work has been carried out in the direction of system reliability and performance evaluation but most of problems either studied under conventional approach or computational methodology is very complex and difficult. But, no simple methodology found in the literature for performance evaluation of engineering systems like paint manufacturing plants.

## SYSTEM DESCRIPTION

In this section, a detailed description of paint manufacturing plant has been appended. The system consists of five subsystems named as mixer (A), grinding mill (B), dilution (C), Labeling Machine (D) and filling machine (E). The subsystem A, B and C are working on configuration 1-out-of-1: good policy while D and E comprises two units each working in parallel configuration. Repair of the system is considered perfect and sufficient repair facilities are available as and when required. All the failure and repair rates are taken as constant. Chapman-Kolmogorov differential equation developed using mnemonic rule and their numerical solution have been obtained using Runge–Kutta method of order four. The required data for estimation of various failure and repair rates are collected with the help of the maintenance personnel of the paint manufacturing plant situated at Jaipur, India. The flow chart and state transition diagram of paint manufacturing plant are shown in figure-1& 2 respectively.



**Figure 1: Reliability Block Diagram of the System**

## MATERIAL AND METHODS

### Notations

| Symbols                         | Description   |
|---------------------------------|---|
| A, B, C, D, E                   | Working states of the System  |
| D <sub>2</sub> , E <sub>2</sub> | Both units in subsystem D and E are in working condition                              |
| D <sub>1</sub> , E <sub>1</sub> | Subsystem D and E are in working condition with one failed unit with reduced capacity |
| a, b, c, d, e                   | Failed states   |
| C                               | Coverage factor   |

|   |   |
|---|---|
| $\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5$ | Failure rates of subsystems A, B, C, D, E                   |
| $\lambda_6, \lambda_7$                                  | Failure rates of subsystems D, E in reduced capacity        |
| $\mu_1, \mu_2, \mu_3, \mu_4, \mu_5$                     | Repair rates of subsystems A, B, C, D, E                    |
| $\mu_6, \mu_7$  | Repair rates of subsystems D, E in reduced capacity         |
| $P_i(t)$  | Probability that the system is in $i^{th}$ state at time t. |

### Failure Rate

The ratio of the number of failure of a component in a given time period to the total time period during which system remains operative is termed as constant failure rate ( $\lambda_i$ ). It is expresses as the number of failures per unit time.

### Repair Rate

The ratio of the number of repairs of a component in a given time period to the total time period during which system repaired is termed as constant repair rate ( $\mu_i$ ). It is expresses as the number of repairs per unit time.

### Fuzzy set

Cai (1996) defined the fuzzy sets as a mathematical tool to investigate the real world systems fuzziness. Let  $x \in X$  be an element of a conventional set then fuzzy set has been defined as a ordered pair of the element and the corresponding membership function over the interval [0, 1].

Mathematically  $A = \{x, \mu_A(x)\}$  over [0, 1]

### Membership Function

Let  $A = \{a_1, a_2, a_3 \dots a_n\}$  be a set of possible states. Let  $x_{s_i} : a_i \rightarrow [0, 1]; x_{F_i} : a_i \rightarrow [0, 1]$ . The  $\{x_{s_i}\}$  represent the success variable and  $\{x_{F_i}\}$  represent failure variable. A new function defined as follows:

$$\mu_s = \mu_s(x_{s_1}, x_{s_2}, \dots, x_{s_n}) : [0, 1]^n \rightarrow [0, 1]; \mu_F = \mu_F(x_{F_1}, x_{F_2}, \dots, x_{F_n}) : [0, 1]^n \rightarrow [0, 1]$$

The function  $\mu_s$  is termed as success membership function and  $\mu_F$  is the failure membership function. By keeping in mind the complexity of the system, membership function for success is defined as the ratio of operative number of components to the total number of components while, for failure it is defined as the ratio of failed number of components to the total number of components.

### Profust Reliability

Cai(1996) defined the profust reliability as

$$\begin{aligned} R(t_0, t_0 + t) &= P\{T_{SF} \text{ doesn't occur during the interval } (t_0, t_0 + T)\} \\ &= 1 - \sum_{i=1}^n \sum_{j=1}^n \mu_{TSF}(m_{ij}) P\{m_{ij} \text{ occurs during } (t_0, t_0 + T)\} \end{aligned}$$

Where  $m_{ij}$  is confined to be the transition from state  $S_i$  to state  $S_j$  without passing via any intermediate state

### Fuzzy Availability

Kumar and Kumar (2011) stated a fuzzy probabilistic semi- Markov model  $\{(S_n, T_n), n \in \mathbb{N}\}$  consisting of 'n' states together with transition time. Let  $U = \{S_1, S_2, \dots, S_n\}$  denote the universe of discourse. On this universe, we define a fuzzy success state  $S$ ,  $S = \{(S_i, \mu_S(S_i)); i = 1, 2, \dots, n\}$  and a fuzzy failure state  $F$ ,  $F = \{(S_i, \mu_F(S_i)); i = 1, 2, \dots, n\}$ , where  $\mu_S(S_i)$  and  $\mu_F(S_i)$  are trapezoidal fuzzy numbers, respectively. The fuzzy availability of the system is defined as

$$A(t) = \sum_{i=1}^k \mu_S(S_i) P_i(t), \text{ where } k \text{ denotes the operative states}$$

### Markov Process

If the state of the system is probability based, the model is a Markov probability model. The fundamental assumption in Markov process is that, the probability  $P_{ij}$ , depends entirely on states  $S_i$  and  $S_j$ , and is independent of all previous states except the last one state  $S_i$ .

### Coverage factor

Kumar and Kumar (2011) stated that the probability of successful reconfiguration operation of a fault-tolerant system is defined as a coverage factor. It is denoted by 'c' and if its value is less than 1, then it is known as imperfect coverage.

### Profit function

No one can expect the survival of any industrial if it perform in loss for a long time. The expected performance of the industry in steady state can be measured by its expected profit, i.e., by the difference of revenue generated per unit time and expenditure per unit time. Mathematically,  $\text{Profit} = R_0 FA - R_1 BP$

Where  $R_0$  denotes the generated revenue per unit time and  $R_1$  is the per unit expenditure for various repair activities. Here,  $FA$  and  $BP$  have been earlier defined.

### ASSUMPTIONS

The following assumptions are taken to perform this study

- The failure and repair rates are constant.
- All time dependent random variables are statistically independent.
- Sufficient repair facility available as and when required immediately.
- At the initial time all unit are operative.
- The system works in reduced capacity upon failure of one parallel unit.
- Repair are perfect.

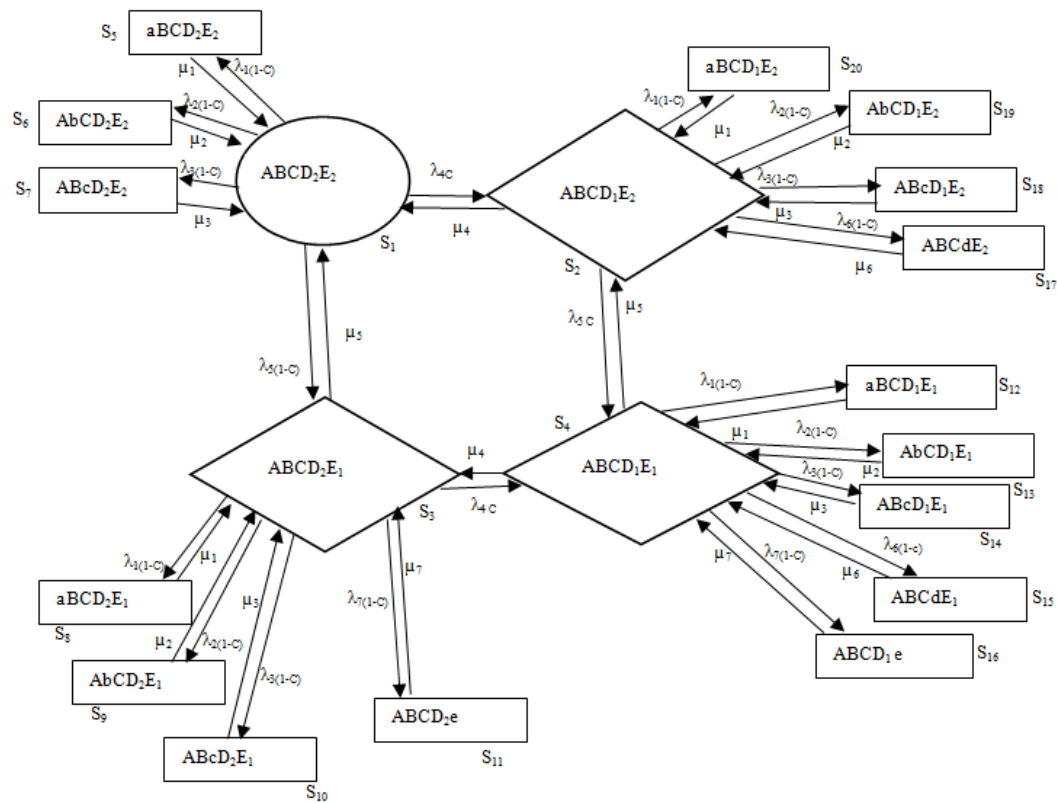


Figure 2: State Transition Diagram

### 3. FORMULATION OF MATHEMATICAL MODEL AND ITS SOLUTION

In this section, a mathematical modeling is formulated for the system described above by using Markov birth-death process for the three subsystems and the Chapman-Kolmogorov equations are derived. The C-K equations are as follows

$$\begin{aligned} \frac{dP_1(t)}{dt} + [(1-c)\lambda_1 + (1-c)\lambda_2 + (1-c)\lambda_3 + c\lambda_4 + (1-c)\lambda_5]P_1(t) \\ = \mu_1P_5(t) + \mu_2P_6(t) + \mu_3P_7(t) + \mu_4P_2(t) + \mu_5P_3(t) \end{aligned} \quad (1)$$

$$\begin{aligned} \frac{dP_2(t)}{dt} + [(1-c)\lambda_1 + (1-c)\lambda_2 + (1-c)\lambda_3 + (1-c)\lambda_6 + c\lambda_5 + \mu_4]P_2(t) \\ = c\lambda_4P_1(t) + \mu_1P_{20}(t) + \mu_2P_{19}(t) + \mu_3P_{18}(t) + \mu_6P_{17}(t) + \mu_5P_4(t) \end{aligned} \quad (2)$$

$$\begin{aligned} \frac{dP_3(t)}{dt} + [(1-c)\lambda_1 + (1-c)\lambda_2 + (1-c)\lambda_3 + (1-c)\lambda_7 + c\lambda_4 + \mu_5]P_3(t) \\ = (1-c)\lambda_5P_1(t) + \mu_1P_8(t) + \mu_2P_9(t) + \mu_4P_4(t) + \mu_7P_{11}(t) + \mu_3P_{10}(t) \end{aligned} \quad (3)$$

$$\begin{aligned} \frac{dP_4(t)}{dt} + [\mu_4 + \mu_5 + (1-c)\lambda_1 + (1-c)\lambda_2 + (1-c)\lambda_6 + (1-c)\lambda_3 + (1-c)\lambda_7]P_4(t) \\ = c\lambda_4P_3(t) + c\lambda_5P_2(t) + \mu_1P_{12}(t) + \mu_2P_{13}(t) + \mu_3P_{14}(t) + \mu_6P_{15}(t) + \mu_7P_{16}(t) \end{aligned} \quad (4)$$

$$\frac{dP_5(t)}{dt} + \mu_1 P_5(t) = (1-c)\lambda_1 P_1(t) \quad (5)$$

$$\frac{dP_6(t)}{dt} + \mu_2 P_6(t) = (1-c)\lambda_2 P_1(t) \quad (6)$$

$$\frac{dP_7(t)}{dt} + \mu_3 P_7(t) = (1-c)\lambda_3 P_1(t) \quad (7)$$

$$\frac{dP_8(t)}{dt} + \mu_1 P_8(t) = (1-c)\lambda_1 P_3(t) \quad (8)$$

$$\frac{dP_9(t)}{dt} + \mu_2 P_9(t) = (1-c)\lambda_2 P_3(t) \quad (9)$$

$$\frac{dP_{10}(t)}{dt} + \mu_3 P_{10}(t) = (1-c)\lambda_3 P_3(t) \quad (10)$$

$$\frac{dP_{11}(t)}{dt} + \mu_7 P_{11}(t) = (1-c)\lambda_7 P_3(t) \quad (11)$$

$$\frac{dP_{12}(t)}{dt} + \mu_1 P_{12}(t) = (1-c)\lambda_1 P_4(t) \quad (12)$$

$$\frac{dP_{13}(t)}{dt} + \mu_2 P_{13}(t) = (1-c)\lambda_2 P_4(t) \quad (13)$$

$$\frac{dP_{14}(t)}{dt} + \mu_3 P_{14}(t) = (1-c)\lambda_3 P_4(t) \quad (14)$$

$$\frac{dP_{15}(t)}{dt} + \mu_6 P_{15}(t) = (1-c)\lambda_6 P_4(t) \quad (15)$$

$$\frac{dP_{16}(t)}{dt} + \mu_7 P_{16}(t) = (1-c)\lambda_7 P_4(t) \quad (16)$$

$$\frac{dP_{17}(t)}{dt} + \mu_6 P_{17}(t) = (1-c)\lambda_6 P_2(t) \quad (17)$$

$$\frac{dP_{18}(t)}{dt} + \mu_3 P_{18}(t) = (1-c)\lambda_3 P_2(t) \quad (18)$$

$$\frac{dP_{19}(t)}{dt} + \mu_2 P_{19}(t) = (1-c)\lambda_2 P_2(t) \quad (19)$$

$$\frac{dP_{20}(t)}{dt} + \mu_1 P_{20}(t) = (1-c)\lambda_1 P_2(t) \quad (20)$$

$$\text{Initial Condition } P_i(0) = \begin{cases} 1 & \text{if } i = 0 \\ 0 & \text{if } i \neq 0 \end{cases} \quad (21)$$

The system of differential equations (1) to (20) along with initial conditions given in equation (21) was solved by Runge-Kutta fourth-order method. The fuzzy availability and fuzzy profit of the paint manufacturing plant is computed for time 60-360 days. In the numerical computation, it is considered that the failure and repair rates of labeling and filling subsystems are different. The data concerning the failure and repair rates are taken from plant persons as follows:

**Table 1: Various Failure and Repair Rates**

| Name of Subsystem        | Failure rate ( $\lambda_i$ ) | Repair rate ( $\mu_i$ ) |
|--------------------------|------------------------------|-------------------------|
| Mixer                    | $\lambda_1 = 0.005$          | $\mu_1 = 0.889$         |
| Grinding mill            | $\lambda_2 = 0.051$          | $\mu_2 = 1.397$         |
| Dilution                 | $\lambda_3 = 0.0052$         | $\mu_3 = 0.998$         |
| Labeling                 | $\lambda_4 = 0.0727$         | $\mu_4 = 1.232$         |
| Filling                  | $\lambda_5 = 0.0954$         | $\mu_5 = 1.244$         |
| Standby Labeling Machine | $\lambda_6 = 0.0778$         | $\mu_6 = 1.374$         |
| Standby Filling Machine  | $\lambda_7 = 0.0955$         | $\mu_7 = 1.387$         |

#### Fuzzy Availability

$$FA = P_1(t) + \frac{6}{7}P_2(t) + \frac{6}{7}P_3(t) + \frac{5}{7}P_4(t) \quad (22)$$

Fuzzy Busy Period:

$$\begin{aligned} FBP = & \frac{1}{7}P_2(t) + \frac{1}{7}P_3(t) + \frac{2}{7}P_4(t) + \frac{1}{7}P_5(t) + \frac{1}{7}P_6(t) + \frac{1}{7}P_7(t) + \frac{2}{7}P_8(t) + \frac{2}{7}P_9(t) + \frac{2}{7}P_{10}(t) \\ & + \frac{2}{7}P_{11}(t) + \frac{3}{7}P_{12}(t) + \frac{3}{7}P_{13}(t) + \frac{3}{7}P_{14}(t) + \frac{3}{7}P_{15}(t) + \frac{3}{7}P_{16}(t) + \frac{2}{7}P_{17}(t) + \frac{2}{7}P_{18}(t) + \frac{2}{7}P_{19}(t) \\ & + \frac{2}{7}P_{20}(t) \end{aligned} \quad (23)$$

Fuzzy profit Function:

$$FP = 50000 * (FA) - 5000 * (FBP) \quad (24)$$

#### Performance Analysis

In this section, the fuzzy availability, fuzzy busy period and fuzzy profit function of the system are computed using equations (22) - (24) respectively. The effect of change of various failure and repair rate of subsystems and coverage factor on these measure with respect to time is appended in tables 2-8.

### Effect of Failure and Repair Rate of Subsystem Named Mixer on the Fuzzy Availability and Profit Function

The effect of failure rate of subsystem named mixer on fuzzy availability and profit function of paint manufacturing plant has been studied by varying values as  $\lambda_1 = 0.005$  to  $\lambda_1 = 0.05$  at a repair rate  $\mu_1 = 0.889$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-2. From table-2, it is analyzed that the availability and profit of system model decreases very low with respect to time. This table shows that fuzzy availability and profit decreases 2.75% approximately with the decrease of the coverage factor value C=1 to C=0. While, by increasing the failure rate the value of these measures decrease from 0.99% to 4.61% with respect to coverage factor value except for C=1.

Similarly, repair rate of subsystem named mixer on fuzzy availability and profit function of paint manufacturing plant has been studied by varying values as  $\mu_1 = 0.889$  to  $\mu_1 = 1.2$  at a failure rate  $\lambda_1 = 0.005$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-2. From table-2, it is analyzed that the availability and profit of system model decreases very low with respect to time. This table shows that fuzzy availability and profit increases 0.13% approximately with the decrease of the coverage factor value C=1 to C=0 after increasing the repair rate. It is also noted that increase or decrease failure rate does not shows any effect on fuzzy availability and profit at the state of full coverage, i.e., C=1. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.981865 and 49002.56 respectively.

**Table 2: Effect of Failure and Repair Rates of Mixer on Fuzzy Availability and Profit Function**

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Mixer Unit |                                       |                                      | Profit with Respect to Failure & Repair Rates of Mixer Unit |                                       |                                      |
|-----------------|-------------|---|---------------------------------------|--------------------------------------|---|---------------------------------------|--------------------------------------|
|                 |             | $\mu_1 = 0.889$<br>$\lambda_1 = 0.005$                            | $\mu_1 = 0.889$<br>$\lambda_1 = 0.05$ | $\mu_1 = 1.2$<br>$\lambda_1 = 0.005$ | $\mu_1 = 0.889$<br>$\lambda_1 = 0.005$                      | $\mu_1 = 0.889$<br>$\lambda_1 = 0.05$ | $\mu_1 = 1.2$<br>$\lambda_1 = 0.005$ |
| C=1             | 40          | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 80          | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 120         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 160         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 200         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 240         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 280         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 320         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
|                 | 360         | 0.981865  | 0.981865                              | 0.981865                             | 49002.56  | 49002.56                              | 49002.56                             |
| C=0.8           | 40          | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 80          | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 120         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 160         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 200         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.64                              | 48672.24                             |
|                 | 240         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 280         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 320         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
|                 | 360         | 0.974799  | 0.965132                              | 0.97508                              | 48657.97  | 48167.65                              | 48672.24                             |
| C=0.4           | 40          | 0.963157  | 0.935581                              | 0.963975                             | 48097.67  | 46699.06                              | 48139.16                             |
|                 | 80          | 0.963157  | 0.935581                              | 0.963975                             | 48097.67  | 46699.07                              | 48139.16                             |
|                 | 120         | 0.963157  | 0.935581                              | 0.963975                             | 48097.67  | 46699.06                              | 48139.17                             |



Table 2: Contd.,

|     |     |          |          |          |          |          |          |
|-----|-----|----------|----------|----------|----------|----------|----------|
|     | 160 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.17 |
|     | 200 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.17 |
|     | 240 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.17 |
|     | 280 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.17 |
|     | 320 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.17 |
|     | 360 | 0.963157 | 0.935581 | 0.963975 | 48097.67 | 46699.06 | 48139.16 |
| C=0 | 40  | 0.9548   | 0.910775 | 0.956131 | 47707.69 | 45476.04 | 47776.21 |
|     | 80  | 0.954799 | 0.910768 | 0.95613  | 47707.68 | 45475.66 | 47776.18 |
|     | 120 | 0.954797 | 0.910748 | 0.956159 | 47707.52 | 45475.66 | 47776.65 |
|     | 160 | 0.954796 | 0.910741 | 0.956127 | 47707.49 | 45475.31 | 47775.9  |
|     | 200 | 0.954795 | 0.910736 | 0.956119 | 47707.57 | 45475.03 | 47775.89 |
|     | 240 | 0.954794 | 0.910724 | 0.956103 | 47707.42 | 45474.9  | 47775.79 |
|     | 280 | 0.954793 | 0.910712 | 0.956093 | 47707.37 | 45474.87 | 47775.33 |
|     | 320 | 0.954791 | 0.910703 | 0.956087 | 47707.26 | 45474.78 | 47775.26 |
|     | 360 | 0.95479  | 0.910695 | 0.956065 | 47707.09 | 45474.04 | 47775.21 |

The effect of failure and repair rate of subsystem named Grinding mill on fuzzy availability and profit function of paint manufacturing plant have been studied by varying values as  $\lambda_2 = 0.051$  to  $\lambda_2 = 0.06$  at a repair rate  $\mu_2 = 1.397$  and  $\mu_2 = 1.397$  to  $\mu_2 = 1.92$  at a failure rate  $\lambda_2 = 0.051$  respectively for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-3. From table-3, it is analyzed that the availability and profit of system model decreases very low with respect to time. This table shows that fuzzy availability and profit increases 0.95% approximately with the increase of the repair rate along with coverage factor value C=1 to C=0. However, value of these measures decrease 2.75% with the increase of failure rate. It is also noted that increase or decrease failure rate does not shows any effect on fuzzy availability and profit at the state of full coverage, i. e., C=1. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.981865 and 49002.56 respectively.

Table 3: Effect of Failure and Repair Rates of Grinding Mill  
on Fuzzy Availability and Profit Function

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Grinding Unit |                                       |                                       | Profit with Respect to Failure & Repair Rates of Grinding Unit |                                       |                                       |
|-----------------|-------------|--|---------------------------------------|---------------------------------------|--|---------------------------------------|---------------------------------------|
|                 |             | $\mu_2 = 1.397$<br>$\lambda_2 = 0.051$                               | $\mu_2 = 1.397$<br>$\lambda_2 = 0.06$ | $\mu_2 = 1.92$<br>$\lambda_2 = 0.005$ | $\mu_2 = 1.397$<br>$\lambda_2 = 0.051$                         | $\mu_2 = 1.397$<br>$\lambda_2 = 0.06$ | $\mu_2 = 1.92$<br>$\lambda_2 = 0.005$ |
| C=1             | 40          | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 80          | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 120         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 160         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 200         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 240         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 280         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
| C=0.8           | 320         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 360         | 0.981865   | 0.981865                              | 0.981865                              | 49002.56   | 49002.56                              | 49002.56                              |
|                 | 40          | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 80          | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 120         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 160         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 200         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
| C=0.4           | 240         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 280         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 320         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 360         | 0.974799   | 0.973558                              | 0.976721                              | 48657.97   | 48595.02                              | 48755.46                              |
|                 | 40          | 0.963157   | 0.959557                              | 0.968766                              | 48097.67   | 47915.1                               | 48382.18                              |

| Table 3: Contd., |     |          |          |          |          |          |          |
|------------------|-----|----------|----------|----------|----------|----------|----------|
|                  | 80  | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 120 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 160 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 200 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 240 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 280 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 320 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
|                  | 360 | 0.963157 | 0.959557 | 0.968766 | 48097.67 | 47915.1  | 48382.18 |
| C=0              | 40  | 0.9548   | 0.948955 | 0.963969 | 47707.69 | 47411.28 | 48172.7  |
|                  | 80  | 0.954799 | 0.948971 | 0.963968 | 47707.68 | 47411.08 | 48172.65 |
|                  | 120 | 0.954797 | 0.94892  | 0.963954 | 47707.52 | 47411.52 | 48171.97 |
|                  | 160 | 0.954796 | 0.949008 | 0.96395  | 47707.49 | 47411.47 | 48171.76 |
|                  | 200 | 0.954795 | 0.94895  | 0.963956 | 47707.47 | 47411.04 | 48171.55 |
|                  | 240 | 0.954794 | 0.94897  | 0.963958 | 47707.42 | 47411.03 | 48171.44 |
|                  | 280 | 0.954793 | 0.948972 | 0.963956 | 47707.37 | 47410.97 | 48171.26 |
|                  | 320 | 0.954791 | 0.948977 | 0.963957 | 47707.26 | 47410.43 | 48171.18 |
|                  | 360 | 0.95479  | 0.948955 | 0.963969 | 47707.09 | 47410.28 | 48171.07 |

The effect of failure and repair rates of subsystem named Dilution on fuzzy availability and profit function of paint manufacturing plant has been studied by varying values as  $\lambda_3 = 0.0052$  to  $\lambda_3 = 0.061$  at a repair rate  $\mu_3 = 0.998$  and  $\mu_3 = 0.998$  to  $\mu_3 = 1.3$  at a failure rate  $\lambda_3 = 0.0052$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-3. From table-3, it is analyzed that the availability and profit of system model decreases very low with respect to time. This table shows that fuzzy availability and profit increases with the decrease of the coverage factor value C=1 to C=0 and failure rate while, increase with the increase of repair rate. It is also noted that increase or decrease failure rate does not shows any effect on fuzzy availability and profit at the state of full coverage, i.e., C=1. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.981865 and 49002.56 respectively.

**Table 4: Effect of Failure and Repair Rates of Dilution on Fuzzy availability and Profit Function**

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Dilution Unit |  |                                       | Profit with Respect to Failure & Repair Rates of Dilution Unit |  |                                       |
|-----------------|-------------|--|--|---------------------------------------|--|--|---------------------------------------|
|                 |             | $\mu_3 = 0.998$<br>$\lambda_3 = 0.0052$                              | $\mu_3 = 0.998$<br>$\lambda_3 = 0.061$ | $\mu_3 = 1.3$<br>$\lambda_3 = 0.0052$ | $\mu_3 = 0.998$<br>$\lambda_3 = 0.0052$                        | $\mu_3 = 0.998$<br>$\lambda_3 = 0.061$ | $\mu_3 = 1.3$<br>$\lambda_3 = 0.0052$ |
| C=1             | 40          | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 80          | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 120         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 160         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 200         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 240         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 280         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 320         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
| C=0.8           | 360         | 0.981865   | 0.981865                               | 0.981865                              | 49002.56   | 49002.56                               | 49002.56                              |
|                 | 40          | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 80          | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 120         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 160         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 200         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 240         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 280         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 320         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |
|                 | 360         | 0.974799   | 0.964133                               | 0.975033                              | 48657.97   | 48116.93                               | 48669.82                              |

Table 4: Contd.,

|       |     |          |          |          |          |          |          |
|-------|-----|----------|----------|----------|----------|----------|----------|
| C=0.4 | 40  | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.43 | 48132.12 |
|       | 80  | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.42 | 48132.12 |
|       | 120 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.43 | 48132.12 |
|       | 160 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.42 | 48132.12 |
|       | 200 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.43 | 48132.12 |
|       | 240 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.42 | 48132.12 |
|       | 280 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.43 | 48132.12 |
|       | 320 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.42 | 48132.12 |
|       | 360 | 0.963157 | 0.932788 | 0.963836 | 48097.67 | 46557.43 | 48132.12 |
| C=0   | 40  | 0.9548   | 0.906413 | 0.955914 | 47707.69 | 45253.29 | 47763.7  |
|       | 80  | 0.954799 | 0.906406 | 0.955905 | 47707.68 | 45253.94 | 47763.7  |
|       | 120 | 0.954797 | 0.906379 | 0.955899 | 47707.52 | 45252.08 | 47763.43 |
|       | 160 | 0.954796 | 0.906345 | 0.955881 | 47707.49 | 45251.43 | 47763.34 |
|       | 200 | 0.954795 | 0.906316 | 0.955872 | 47707.47 | 45250.94 | 47763.26 |
|       | 240 | 0.954794 | 0.906287 | 0.955863 | 47707.42 | 45250.51 | 47763.16 |
|       | 280 | 0.954793 | 0.906205 | 0.955849 | 47707.37 | 45250.41 | 47763.06 |
|       | 320 | 0.954791 | 0.906192 | 0.955814 | 47707.26 | 45250.33 | 47762.23 |
|       | 360 | 0.95479  | 0.906173 | 0.955804 | 47707.09 | 45250.29 | 47761.7  |

The effect of failure and repair rate of subsystem named labeling machine (when both unit work in parallel) on fuzzy availability and profit function of paint manufacturing plant have been studied by varying values as  $\lambda_4 = 0.0727$  to  $\lambda_4 = 0.8$  at a repair rate  $\mu_4 = 1.232$  and  $\mu_4 = 1.232$  to  $\mu_4 = 1.69$  at a failure rate  $\lambda_4 = 0.0727$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-5. From table-5, it is analyzed that the availability and profit of system model decreases very low with respect to time. This table shows that fuzzy availability and profit increases 0.21% approximately with the decrease of the coverage factor value C=1 to C=0 after increasing the repair rate. However, the availability and profit decline immediately 5.14% with the increase of failure rate of labeling machine. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.983933 and 49116.31 respectively.

Table 5: Effect of Failure and Repair Rates of Labeling Machine  
on Fuzzy availability and Profit Function

| Coverage Factor | Time (days) | Availability with Respect to Failure & Repair Rates of Labeling Unit |                                      |  | Profit with Respect to Failure & Repair Rates of Labeling Unit |                                      |  |
|-----------------|-------------|--|--------------------------------------|--|--|--------------------------------------|--|
|                 |             | $\mu_4 = 1.232$<br>$\lambda_4 = 0.0727$                              | $\mu_4 = 1.232$<br>$\lambda_4 = 0.8$ | $\mu_4 = 1.69$<br>$\lambda_4 = 0.0727$ | $\mu_4 = 1.232$<br>$\lambda_4 = 0.0727$                        | $\mu_4 = 1.232$<br>$\lambda_4 = 0.8$ | $\mu_4 = 1.69$<br>$\lambda_4 = 0.0727$ |
| C=1             | 40          | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 80          | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 120         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 160         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 200         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 240         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 280         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 320         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
|                 | 360         | 0.981865   | 0.933582                             | 0.983933                               | 49002.56   | 46347                                | 49116.31                               |
| C=0.8           | 40          | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 80          | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 120         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 160         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.2                              | 48756.51                               |
|                 | 200         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 240         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 280         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |
|                 | 320         | 0.974799   | 0.929759                             | 0.976597                               | 48657.97   | 46190.19                             | 48756.51                               |

| Table 5: Contd., |     |          |          |          |          |          |          |
|------------------|-----|----------|----------|----------|----------|----------|----------|
|                  | 360 | 0.974799 | 0.929759 | 0.976597 | 48657.97 | 46190.19 | 48756.51 |
| C=0.4            | 40  | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 80  | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 120 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.57 | 48154.69 |
|                  | 160 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 200 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 240 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.57 | 48154.69 |
|                  | 280 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 320 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.57 | 48154.69 |
| C=0              | 360 | 0.963157 | 0.93214  | 0.964204 | 48097.67 | 46408.58 | 48154.69 |
|                  | 40  | 0.9548   | 0.9548   | 0.9548   | 47707.69 | 47707.69 | 47707.69 |
|                  | 80  | 0.954799 | 0.954799 | 0.954799 | 47707.68 | 47707.68 | 47707.68 |
|                  | 120 | 0.954797 | 0.954797 | 0.954797 | 47707.52 | 47707.52 | 47707.52 |
|                  | 160 | 0.954796 | 0.954796 | 0.954796 | 47707.49 | 47707.49 | 47707.49 |
|                  | 200 | 0.954795 | 0.954795 | 0.954795 | 47707.47 | 47707.47 | 47707.47 |
|                  | 240 | 0.954794 | 0.954794 | 0.954794 | 47707.42 | 47707.42 | 47707.42 |
|                  | 280 | 0.954793 | 0.954793 | 0.954793 | 47707.37 | 47707.37 | 47707.37 |
|                  | 320 | 0.954791 | 0.954791 | 0.954791 | 47707.26 | 47707.26 | 47707.26 |
|                  | 360 | 0.95479  | 0.95479  | 0.95479  | 47707.09 | 47707.09 | 47707.09 |

The effect of failure and repair rate of subsystem named filling machine (when both unit work in parallel) on fuzzy availability and profit function of paint manufacturing plant have been studied by varying values as  $\lambda_5 = 0.0954$  to  $\lambda_5 = 0.9$  at a repair rate  $\mu_5 = 1.244$  and  $\mu_5 = 1.244$  to  $\mu_5 = 1.7$  at a failure rate  $\lambda_5 = 0.0954$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-6. From table-6, it is analyzed that the availability and profit of system model decreases very low with respect to time but it rapidly decrease with decrease of the coverage factor value C=1 to C=0. This table shows that fuzzy availability and profit increases 0.26after increasing the repair rate. However, the availability and profit decline immediately 5.34% with the increase of failure rate of filling machine. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.984449 and 49144.69 respectively.

**Table 6: Effect of Failure and Repair Rates of Filling Machine on Fuzzy Availability and Profit Function**

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Filling Unit |                                      |                                       | Profit with Respect to Failure & Repair Rates of Filling Unit |                                      |                                       |
|-----------------|-------------|---|--------------------------------------|---------------------------------------|---|--------------------------------------|---------------------------------------|
|                 |             | $\mu_5 = 1.244$<br>$\lambda_5 = 0.0954$                             | $\mu_5 = 1.244$<br>$\lambda_5 = 0.9$ | $\mu_5 = 1.7$<br>$\lambda_5 = 0.0954$ | $\mu_5 = 1.244$<br>$\lambda_5 = 0.0954$                       | $\mu_5 = 1.244$<br>$\lambda_5 = 0.9$ | $\mu_5 = 1.7$<br>$\lambda_5 = 0.0954$ |
| C=1             | 40          | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 80          | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 120         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 160         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 200         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 240         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 280         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 320         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
|                 | 360         | 0.981865  | 0.932072                             | 0.984449                              | 49002.56  | 46263.95                             | 49144.69                              |
| C=0.8           | 40          | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.59                              |
|                 | 80          | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.58                              |
|                 | 120         | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.59                              |
|                 | 160         | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.58                              |
|                 | 200         | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.59                              |
|                 | 240         | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.58                              |
|                 | 280         | 0.974799  | 0.927255                             | 0.977094                              | 48657.97  | 46055.52                             | 48783.58                              |

Table 6: Contd.,

|       |     |          |          |          |          |          |          |
|-------|-----|----------|----------|----------|----------|----------|----------|
|       | 320 | 0.974799 | 0.927255 | 0.977094 | 48657.97 | 46055.52 | 48783.59 |
|       | 360 | 0.974799 | 0.927255 | 0.977094 | 48657.97 | 46055.52 | 48783.59 |
| C=0.4 | 40  | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 80  | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.11 | 48172.9  |
|       | 120 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 160 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 200 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 240 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 280 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 320 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
|       | 360 | 0.963157 | 0.928917 | 0.964541 | 48097.67 | 46237.12 | 48172.9  |
| C=0   | 40  | 0.9548   | 0.9548   | 0.9548   | 47707.69 | 47707.69 | 47707.69 |
|       | 80  | 0.954799 | 0.954799 | 0.954799 | 47707.68 | 47707.68 | 47707.68 |
|       | 120 | 0.954797 | 0.954797 | 0.954797 | 47707.52 | 47707.52 | 47707.52 |
|       | 160 | 0.954796 | 0.954796 | 0.954796 | 47707.49 | 47707.49 | 47707.49 |
|       | 200 | 0.954795 | 0.954795 | 0.954795 | 47707.47 | 47707.47 | 47707.47 |
|       | 240 | 0.954794 | 0.954794 | 0.954794 | 47707.42 | 47707.42 | 47707.42 |
|       | 280 | 0.954793 | 0.954793 | 0.954793 | 47707.37 | 47707.37 | 47707.37 |
|       | 320 | 0.954791 | 0.954791 | 0.954791 | 47707.26 | 47707.26 | 47707.26 |
|       | 360 | 0.95479  | 0.95479  | 0.95479  | 47707.09 | 47707.09 | 47707.09 |

The effect of failure and repair rate of subsystem named labeling machine (when only standby unit is operative) on fuzzy availability and profit function of paint manufacturing plant has been studied by varying values as  $\lambda_6 = 0.0778$  to  $\lambda_6 = 0.72$  at a repair rate  $\mu_6 = 1.374$  and  $\mu_6 = 1.374$  to  $\mu_6 = 1.89$  at a failure rate  $\lambda_6 = 0.0778$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-7. From table-7, it is analyzed that the availability and profit of system model decreases very low with respect to time, but very rapidly with respect to coverage factor. This table shows that fuzzy availability and profit increases with increase of the repair rate. However, the availability and profit decline immediately with the increase of failure rate of standby labeling machine. It is also noted that increase or decrease failure rate does not shows any effect on fuzzy availability and profit at the state of full coverage, i.e., C=1. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.981865 and 49002.56 respectively.

Table 7: Effect of Failure and Repair Rates of Standby Labeling Machine  
on Fuzzy Availability and Profit Function

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Standby Labeling Unit |                                       |  | Profit with Respect to Failure & Repair Rates of Standby Labeling Unit |                                       |  |
|-----------------|-------------|--|---------------------------------------|--|--|---------------------------------------|--|
|                 |             | $\mu_6 = 1.374$<br>$\lambda_6 = 0.0778$                                      | $\mu_6 = 1.374$<br>$\lambda_6 = 0.72$ | $\mu_6 = 1.89$<br>$\lambda_6 = 0.0778$ | $\mu_6 = 1.374$<br>$\lambda_6 = 0.0778$                                | $\mu_6 = 1.374$<br>$\lambda_6 = 0.72$ | $\mu_6 = 1.89$<br>$\lambda_6 = 0.0778$ |
| C=1             | 40          | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 80          | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 120         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 160         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 200         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 240         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 280         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 320         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
| C=0.8           | 360         | 0.981865   | 0.981865                              | 0.981865                               | 49002.56   | 49002.56                              | 49002.56                               |
|                 | 40          | 0.974799   | 0.970752                              | 0.974933                               | 48657.97   | 48449.86                              | 48664.89                               |
|                 | 80          | 0.974799   | 0.970752                              | 0.974933                               | 48657.97   | 48449.85                              | 48664.89                               |
|                 | 120         | 0.974799   | 0.970752                              | 0.974933                               | 48657.97   | 48449.86                              | 48664.89                               |
|                 | 160         | 0.974799   | 0.970752                              | 0.974933                               | 48657.97   | 48449.86                              | 48664.89                               |

| Table 7: Contd., |     |          |          |          |          |          |          |
|------------------|-----|----------|----------|----------|----------|----------|----------|
|                  | 200 | 0.974799 | 0.970752 | 0.974933 | 48657.97 | 48449.85 | 48664.89 |
|                  | 240 | 0.974799 | 0.970752 | 0.974933 | 48657.97 | 48449.85 | 48664.89 |
|                  | 280 | 0.974799 | 0.970752 | 0.974933 | 48657.97 | 48449.86 | 48664.89 |
|                  | 320 | 0.974799 | 0.970752 | 0.974933 | 48657.97 | 48449.85 | 48664.89 |
|                  | 360 | 0.974799 | 0.970752 | 0.974933 | 48657.97 | 48449.86 | 48664.89 |
| C=0.4            | 40  | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.96 |
|                  | 80  | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.66 | 48107.96 |
|                  | 120 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.96 |
|                  | 160 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.66 | 48107.96 |
|                  | 200 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.66 | 48107.95 |
|                  | 240 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.96 |
|                  | 280 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.95 |
|                  | 320 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.96 |
|                  | 360 | 0.963157 | 0.95715  | 0.963357 | 48097.67 | 47788.65 | 48107.96 |
| C=0              | 40  | 0.9548   | 0.9548   | 0.9548   | 47707.69 | 47707.69 | 47707.69 |
|                  | 80  | 0.954799 | 0.954799 | 0.954799 | 47707.68 | 47707.68 | 47707.68 |
|                  | 120 | 0.954797 | 0.954797 | 0.954797 | 47707.52 | 47707.52 | 47707.52 |
|                  | 160 | 0.954796 | 0.954796 | 0.954796 | 47707.49 | 47707.49 | 47707.49 |
|                  | 200 | 0.954795 | 0.954795 | 0.954795 | 47707.47 | 47707.47 | 47707.47 |
|                  | 240 | 0.954794 | 0.954794 | 0.954794 | 47707.42 | 47707.42 | 47707.42 |
|                  | 280 | 0.954793 | 0.954793 | 0.954793 | 47707.37 | 47707.37 | 47707.37 |
|                  | 320 | 0.954791 | 0.954791 | 0.954791 | 47707.26 | 47707.26 | 47707.26 |
|                  | 360 | 0.95479  | 0.95479  | 0.95479  | 47707.09 | 47707.09 | 47707.09 |

The effect of failure and repair rate of subsystem named filling machine (when only standby unit is operative) on fuzzy availability and profit function of paint manufacturing plant has been studied by varying values as  $\lambda_f = 0.0955$  to  $\lambda_f = 0.94$  at a repair rate  $\mu_f = 1.387$  and  $\mu_f = 1.387$  to  $\mu_f = 1.9$  at a failure rate  $\lambda_f = 0.0955$  for different values of coverage factor 'C'. The failure and repair rates of other subsystems have been taken constant as given in table-1. The numerical results of fuzzy availability and profit function of system based on this data is appended in table-8. From table-8, it is analyzed that the availability and profit of system model decreases very low with respect to time, but very rapidly with respect to coverage factor. This table shows that fuzzy availability and profit increases with increase of the repair rate. However, the availability and profit decline immediately with the increase of failure rate of standby labeling machine. It is also noted that increase or decrease failure rate does not shows any effect on fuzzy availability and profit at the state of full coverage, i.e., C=1. Finally, we conclude that the maximum value of fuzzy availability and profit are 0.981865 and 49002.56 respectively.

**Table 8: Effect of Failure and Repair Rates of Standby Filling Machine on Fuzzy Availability and Profit Function**

| Coverage Factor | Time (Days) | Availability with Respect to Failure & Repair Rates of Standby Filling Unit |                                       |                                       | Profit with Respect to Failure & Repair Rates of Standby Filling Unit |                                       |                                       |
|-----------------|-------------|---|---------------------------------------|---------------------------------------|---|---------------------------------------|---------------------------------------|
|                 |             | $\mu_f = 1.387$<br>$\lambda_f = 0.0955$                                     | $\mu_f = 1.387$<br>$\lambda_f = 0.94$ | $\mu_f = 1.9$<br>$\lambda_f = 0.0955$ | $\mu_f = 1.387$<br>$\lambda_f = 0.0955$                               | $\mu_f = 1.387$<br>$\lambda_f = 0.94$ | $\mu_f = 1.9$<br>$\lambda_f = 0.0955$ |
| C=1             | 40          | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 80          | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 120         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 160         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 200         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 240         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 280         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 320         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
| C=0.8           | 360         | 0.981865  | 0.981865                              | 0.981865                              | 49002.56  | 49002.56                              | 49002.56                              |
|                 | 40          | 0.974799  | 0.968057                              | 0.975006                              | 48657.97  | 48311.36                              | 48668.63                              |
|                 | 80          | 0.974799  | 0.968057                              | 0.975006                              | 48657.97  | 48311.36                              | 48668.63                              |



Table 8: Contd.,

|       |     |          |          |          |          |          |          |
|-------|-----|----------|----------|----------|----------|----------|----------|
|       | 120 | 0.974799 | 0.968057 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 160 | 0.974799 | 0.968057 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 200 | 0.974799 | 0.968058 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 240 | 0.974799 | 0.968058 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 280 | 0.974799 | 0.968057 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 320 | 0.974799 | 0.968057 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
|       | 360 | 0.974799 | 0.968057 | 0.975006 | 48657.97 | 48311.36 | 48668.63 |
| C=0.4 | 40  | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 80  | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 120 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 160 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.63 |
|       | 200 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 240 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.63 |
|       | 280 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 320 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
|       | 360 | 0.963157 | 0.9531   | 0.963467 | 48097.67 | 47580.36 | 48113.64 |
| C=0   | 40  | 0.9548   | 0.9548   | 0.9548   | 47707.69 | 47707.69 | 47707.69 |
|       | 80  | 0.954799 | 0.954799 | 0.954799 | 47707.68 | 47707.68 | 47707.68 |
|       | 120 | 0.954797 | 0.954797 | 0.954797 | 47707.52 | 47707.52 | 47707.52 |
|       | 160 | 0.954796 | 0.954796 | 0.954796 | 47707.49 | 47707.49 | 47707.49 |
|       | 200 | 0.954795 | 0.954795 | 0.954795 | 47707.47 | 47707.47 | 47707.47 |
|       | 240 | 0.954794 | 0.954794 | 0.954794 | 47707.42 | 47707.42 | 47707.42 |
|       | 280 | 0.954793 | 0.954793 | 0.954793 | 47707.37 | 47707.37 | 47707.37 |
|       | 320 | 0.954791 | 0.954791 | 0.954791 | 47707.26 | 47707.26 | 47707.26 |
|       | 360 | 0.95479  | 0.95479  | 0.95479  | 47707.09 | 47707.09 | 47707.09 |

## CONCLUSIONS

The fuzzy availability and performance analysis of paint manufacturing plant discussed above can play a key role in increasing the production of the plant. From the above analysis, it explores that coverage factor has a prominent role in the fuzzy availability and profit of the system. A critical and comparative analysis shows that labeling machine and filling machine unit have a prominent effect on the system in comparison to other units. Finally, it is conclude that by improving the process of fault coverage, increasing the repair rate of labeling unit, increasing the repair rate of filling unit and adopting proper maintenance policies the fuzzy availability and profit function will be improved.

## REFERENCES

1. Aggarwal, A. K., Kumar, S., & Singh, V. (2016). Mathematical modeling and fuzzy availability analysis for serial processes in the crystallization system of a sugar plant. *Journal of Industrial Engineering International*, 1-12
2. Aggarwal, A. K., Singh, V., & Kumar, S. (2014). Availability analysis and performance optimization of a butter oil production system: a case study. *International Journal of System Assurance Engineering and Management*, 8(1), 538-554
3. Aliev, I. M., & Kara, Z. (2004). Fuzzy system reliability analysis using time dependent fuzzy set. *Control and Cybernetics*, 33(4), 653-662
4. Barlow, R. E. Proschan (1965)" *Mathematical Theory of Reliability*. John Wiley& Sons Inc., New York.
5. Cai, K. Y., Wen, C. Y., & Zhang, M. L. (1993). Fuzzy states as a basis for a theory of fuzzy reliability. *Microelectronics Reliability*, 33(15), 2253-2263
6. Cai, K. Y. (1996). *Introduction to Fuzzy Reliability*. Kluwer Academic Publishers. Norwell, MA, USA
7. Chen, S. M. (1994). Fuzzy system reliability analysis using fuzzy number arithmetic operations. *Fuzzy sets and systems*, 64(1), 31-38

8. Chen, S. M. (2003). Analyzing fuzzy system reliability using vague set theory. *International Journal of Applied Science and Engineering*, 1(1), 82-88
9. Jiang, M., Zhou, J., Hu, M., & Ding, Y. (2007, November). Fuzzy reliability of mirrored disk organizations. In *Convergence Information Technology, 2007. International Conference on* (pp. 1345-1348). IEEE
10. Kumar, K., & Kumar, P. (2011). Fuzzy availability modeling and analysis of biscuit manufacturing plant: a case study. *International Journal of System Assurance Engineering and Management*, 2(3), 193-204
11. Kumar, A., & Malik, S. C. (2014). Reliability Modelling of a Computer System with Priority to H/W Repair over Replacement of H/W and Up-gradation of S/W Subject to MOT and MRT. *Jordan Journal of Mechanical and Industrial Engineering*, 8(4), pp. 233-241
12. Mahrous, A. (2013). Thermal performance of PCM based heat sinks. *Int J Mech Eng*, 2(4)
13. Kaufmann, A. (1975). *Introduction to the theory of fuzzy subsets* (Vol. 2). Academic Pr
14. Singer, D. (1990). A fuzzy set approach to fault tree and reliability analysis. *Fuzzy sets and systems*, 34(2), 145-15
15. Sharma, G., & Khanduja, R. (2013). Performance evaluation and availability analysis of feeding system in a sugar industry. *Int J Res EngApplSci*, 3(9), 38-50
16. Zadeh, L. A. (1965). Fuzzy sets. *Information and control*, 8(3), 338-353
17. Zuang, H. Z. (1995). Reliability analysis method in the presence of fuzziness attached to operating time. *Microelectronics Reliability*, 35(12), 1483-1487
18. Ram, M. (2013). On system reliability approaches: A brief survey. *International Journal of Systems Assurance Engineering and Management*, 4(2):101–117.
19. Li, Zhi-Gang and Zhou, Jun-Gang and Liu, Bo-Ying (2017). System Reliability Analysis Method Based on Fuzzy Probability, *International Journal of Fuzzy Systems*, 19(6), 1759-1767.
20. Komal, Sharma SP, Kumar D (2009) Stochastic behavior analysis of the press unit in a paper mill using GABLT technique. *Int. J. Intell. Comput. Cybern.* 2(3):574–593
21. Komal, Sharma SP, Kumar D (2010) RAM analysis of repairable industrial systems utilizing uncertain data. *Appl. Soft. Comput.*, 10:1208–1221
22. Prasath, K. A., & Johnson, R. D. J. Scrutiny of Machine Assignment in Various Intra-Cell Layout in Cellular Manufacturing using Automation Studios
23. Kumar N, Borm JH, Kumar A (2012) Reliability analysis of waste clean-up manipulator using genetic algorithms and fuzzy methodology. *ComputOper Res* 39(2):310–319
24. Kumar, A. & Saini, M. (2017). Mathematical modeling of sugar plant: a fuzzy approach. *Life Cycle Reliability and Safety Engineering*. <https://doi.org/10.1007/s41872-017-0038-0>
25. Kumar, A. & Saini, M. (2018). Stochastic Modeling and Cost-Benefit Analysis of Computing Device with Fault Detection Subject to Expert Repair Facility *Int. j. inf. tecnol.* <https://doi.org/10.1007/s41870-018-0082-7>
26. Mishra KB (1992) *Reliability analysis and prediction: a methodology oriented treatment*. Elsevier, Amsterdam
27. Sharma S.P., Vishwakarma Y. (2014), "Availability optimization of Refining System of Sugar Industry by Markov Process and Genetic Algorithm", *International Conference on Reliability, optimization and Information Technology, India*, 29-33



28. Kachitvichyanukul, V., "Comparison of Three Evolutionary Algorithms: GA, PSO, and DE", *Industrial Engineering & Management Systems*, Vol. 11, (2012), No. 3, 215-223
29. Cui, L., and M. Xie. 2001. Availability analysis of periodically inspected systems with random walk model. *Journal of Applied Probability* 38:860–71. doi:10.1017/S0021900200019082
30. Qingan Qiu & Lirong Cui (2018): Availability analysis for general repairable systems with repair time threshold, *Communications in Statistics - Theory and Methods*, DOI: 10.1080/03610926.2017.1417430

